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LECTURE

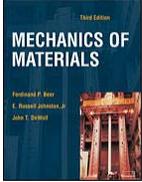


3

Chapter
2.8

RODS: AXIAL LOADING AND DEFORMATION

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ENES 220 – Mechanics of Materials
Department of Civil and Environmental Engineering
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LECTURE 3. RODS: AXIAL LOADING AND DEFORMATION (2.8)
Slide No. 1



Deformations of Members under Axial Loading

- Uniform Member
 - Consider a homogeneous rod as shown in the figure of the next viewgraph.
 - If the resultant axial stress $\sigma = P/A$ does not exceed the proportional limit of the material, then Hooke's law can be applied, that is

$$\sigma = E\varepsilon$$

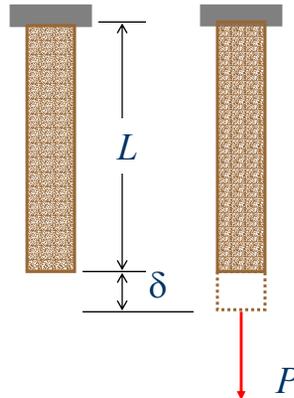
σ = axial stress, ε = axial strain
 E = modulus of elasticity





Deformations of Members under Axial Loading

■ Uniform Member



Deformations of Members under Axial Loading

■ Uniform Member

– From Hooke's law, it follows that

$$\sigma = E\varepsilon \quad (\text{Hooke's law})$$

$$\frac{P}{A} = E\varepsilon$$

But $\varepsilon = \frac{\delta}{L}$, therefore,

$$\frac{P}{A} = E \frac{\delta}{L} \Rightarrow \delta = \frac{PL}{EA}$$



Deformations of Members under Axial Loading

- Uniform Member
 - The deflection (deformation), δ , of the uniform member subjected to axial loading P is given by

$$\delta = \frac{PL}{EA} \quad (1)$$



Deformations of Members under Axial Loading

- Multiple Loads/Sizes
 - The expression for the deflection of the previous equation may be used only if the rod or the member is homogeneous (constant E) and has a uniform cross sectional area A , and is loaded at its ends.
 - If the member is loaded at other points, or if it consists of several portions of various cross sections, and materials, then



Deformations of Members under Axial Loading

■ Multiple Loads/Sizes

- It needs to be divided into components which satisfy individually the required conditions for application of the formula.
- Denoting respectively by P_i , L_i , A_i , and E_i , the internal force, length, cross-sectional area, and modulus of elasticity corresponding to component i , then

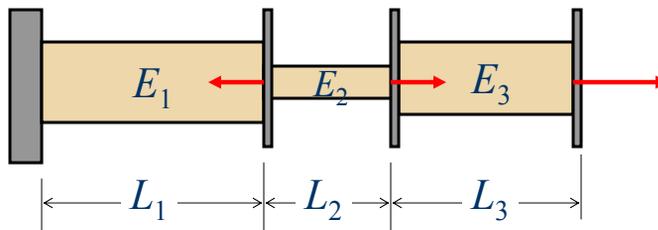
$$\delta = \sum_{i=1}^n \delta_i = \sum_{i=1}^n \frac{P_i L_i}{E_i A_i}$$



Deformations of Members under Axial Loading

■ Multiple Loads/Sizes

$$\delta = \sum_{i=1}^n \delta_i = \sum_{i=1}^n \frac{P_i L_i}{E_i A_i}$$



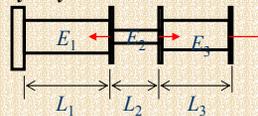


Deformations of Members under Axial Loading

■ Multiple Loads/Sizes

- The deformation of various parts of a rod or uniform member can be given by

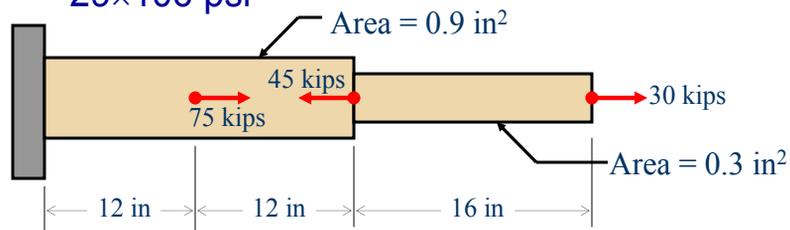
$$\delta = \sum_{i=1}^n \delta_i = \sum_{i=1}^n \frac{P_i L_i}{E_i A_i} \quad (2)$$



Deformations of Members under Axial Loading

■ Example 4

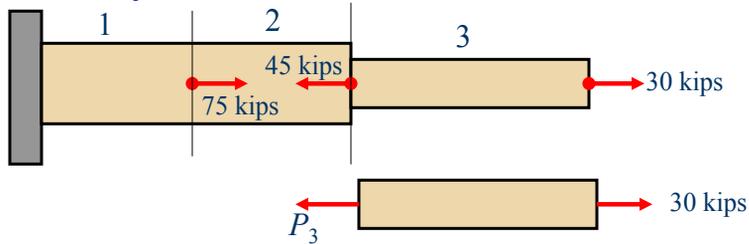
- Determine the deformation of the steel rod shown under the given loads. Assume that the modulus of elasticity for all parts is
- 29×10^6 psi





Deformations of Members under Axial Loading

- Example 4 (cont'd)
 - Analysis of internal forces



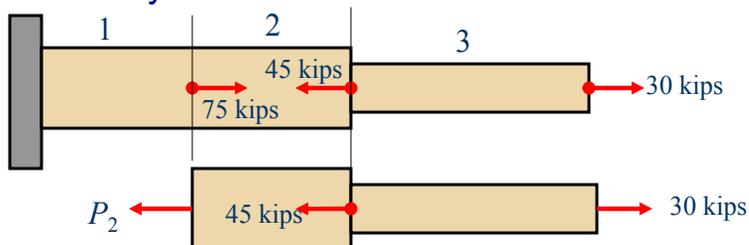
$$\rightarrow + \sum F_x = 0; -P_3 + 30 = 0$$

$$\therefore P_3 = 30 \text{ kips}$$



Deformations of Members under Axial Loading

- Example 4 (cont'd)
 - Analysis of internal forces



$$\rightarrow + \sum F_x = 0; -P_2 - 45 + 30 = 0$$

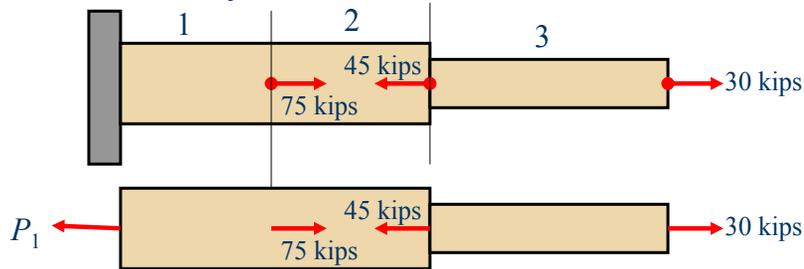
$$\therefore P_2 = -15 \text{ kips}$$



Deformations of Members under Axial Loading

■ Example 4 (cont'd)

– Analysis of internal forces



$$\rightarrow + \sum F_x = 0; -P_1 + 75 - 45 + 30 = 0$$

$$\therefore P_1 = 60 \text{ kips}$$



Deformations of Members under Axial Loading

■ Example 4 (cont'd)

– Deflection

• Input parameters

$$L_1 = 12 \text{ in} \quad L_2 = 12 \text{ in} \quad L_3 = 16 \text{ in}$$

$$A_1 = 0.9 \text{ in}^2 \quad A_2 = 0.9 \text{ in}^2 \quad A_3 = 0.3 \text{ in}^2$$

From analysis of internal forces,

$$P_1 = 60 \text{ kips} = 60,000 \text{ lb}$$

$$P_2 = -15 \text{ kips} = -15,000 \text{ lb}$$

$$P_3 = 30 \text{ kips} = 30,000 \text{ lb}$$



Deformations of Members under Axial Loading

■ Example 4 (cont'd)

– Carrying the values into the deformation formula:

$$\delta = \sum_{i=1}^3 \frac{P_i L_i}{E_i A_i} = \frac{1}{E} \left(\frac{P_1 L_1}{A_1} + \frac{P_2 L_2}{A_2} + \frac{P_3 L_3}{A_3} \right)$$

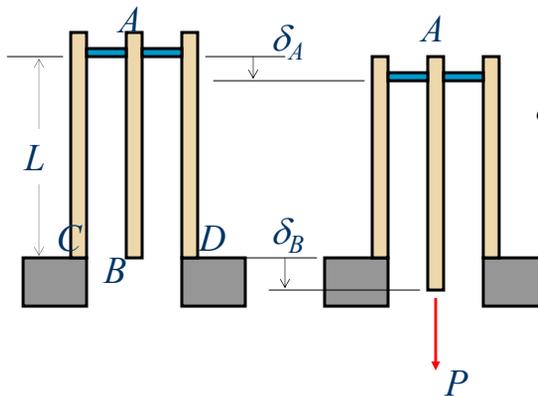
$$\frac{1}{29 \times 10^6} \left(\frac{60,000(12)}{0.9} + \frac{-15,000(12)}{0.9} + \frac{30,000(16)}{0.3} \right)$$

$$\delta = 0.0759 \text{ in}$$



Deformations of Members under Axial Loading

■ Relative Deformation



$$\delta_{B/A} = \delta_B - \delta_A = \frac{PL}{AE}$$



Deformations of Members under Axial Loading

- Relative Deformation
 - If the load P is applied at B , each of the three bars will deform.
 - Since the bars AC and AD are attached to the fixed supports at C and D , their common deformation is measured by the displacement δ_A at point A .



Deformations of Members under Axial Loading

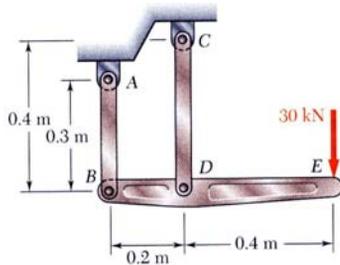
- Relative Deformation
 - On the other hand, since both ends of bars AB move, the deformation of AB is measured by the difference between the displacements δ_A and δ_B of points A and B .
 - That is by relative displacement of B with respect to A , or

$$\delta_{B/A} = \delta_B - \delta_A = \frac{PL}{EA} \quad (3)$$



Deformations of Members under Axial Loading

■ Example 5



The rigid bar BDE is supported by two links AB and CD .

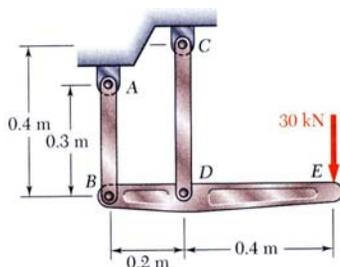
Link AB is made of aluminum ($E = 70$ GPa) and has a cross-sectional area of 500 mm². Link CD is made of steel ($E = 200$ GPa) and has a cross-sectional area of $(600$ mm²).

For the 30 -kN force shown, determine the deflection a) of B , b) of D , and c) of E .



Deformations of Members under Axial Loading

■ Example 5 (cont'd)



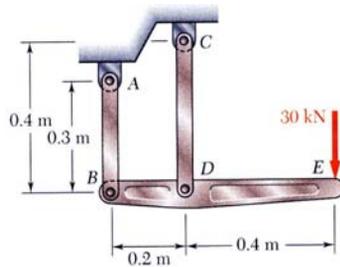
SOLUTION:

- Apply a free-body analysis to the bar BDE to find the forces exerted by links AB and DC .
- Evaluate the deformation of links AB and DC or the displacements of B and D .
- Work out the geometry to find the deflection at E given the deflections at B and D .



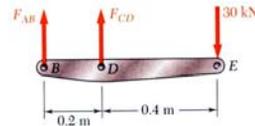
Deformations of Members under Axial Loading

■ Example 5 (cont'd)



SOLUTION:

Free body: Bar BDE



$$\sum M_B = 0$$

$$0 = -(30 \text{ kN} \times 0.6 \text{ m}) + F_{CD} \times 0.2 \text{ m}$$

$$F_{CD} = +90 \text{ kN} \text{ tension}$$

$$\sum M_D = 0$$

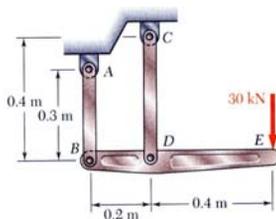
$$0 = -(30 \text{ kN} \times 0.4 \text{ m}) - F_{AB} \times 0.2 \text{ m}$$

$$F_{AB} = -60 \text{ kN} \text{ compression}$$

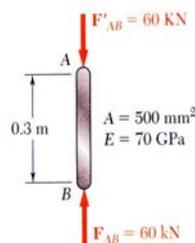


Deformations of Members under Axial Loading

■ Example 5 (cont'd)



Displacement of B:



$$\delta_B = \frac{PL}{AE}$$

$$= \frac{(-60 \times 10^3 \text{ N})(0.3 \text{ m})}{(500 \times 10^{-6} \text{ m}^2)(70 \times 10^9 \text{ Pa})}$$

$$= -514 \times 10^{-6} \text{ m}$$

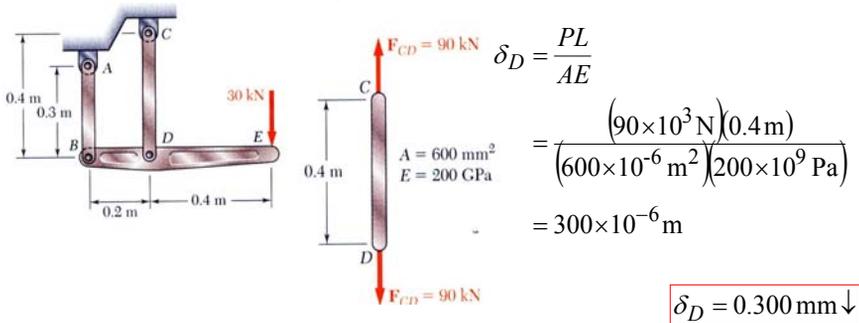
$$\delta_B = 0.514 \text{ mm} \uparrow$$



Deformations of Members under Axial Loading

■ Example 5 (cont'd)

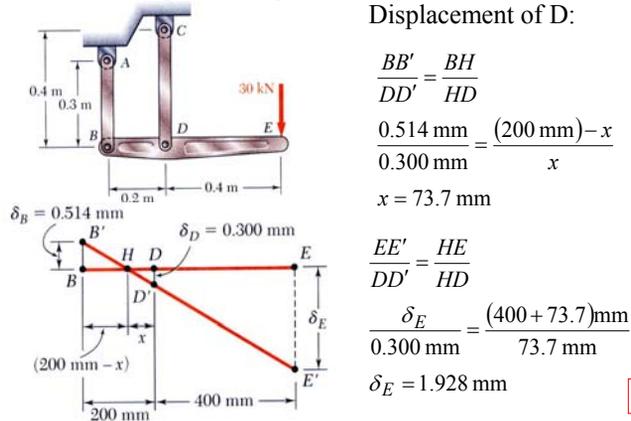
Displacement of D:



Deformations of Members under Axial Loading

■ Example 5 (cont'd)

Displacement of D:





Deformations of Members under Axial Loading

- Nonuniform Deformation
 - For cases in which the axial force or the cross-sectional area varies continuously along the length of the bar, then Eq. 1
 - (PL / EA) is not valid.
 - Recall that in the case of variable cross section, the strain depends on the position of point Q, where it is computed from

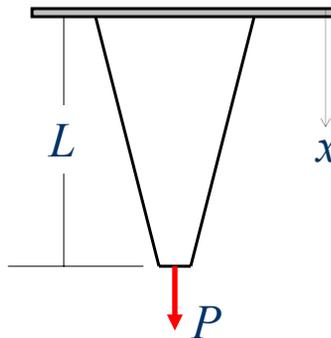
$$\varepsilon = \frac{d\delta}{dx}$$



Deformations of Members under Axial Loading

- Nonuniform Deformation

$$\varepsilon = \frac{d\delta}{dx}$$





Deformations of Members under Axial Loading

- Nonuniform Deformation
 - Solving for $d\delta$ and substituting for ε

$$d\delta = \varepsilon dx$$

- But $\varepsilon = \sigma / E$, and $\sigma = P/A$. therefore

$$d\delta = \varepsilon dx = \frac{\sigma}{E} dx = \frac{P}{EA} dx \quad (4)$$



Deformations of Members under Axial Loading

- Nonuniform Deformation
 - The total deformation δ of the rod or bar is obtained by integrating Eq. 4 over the length L as

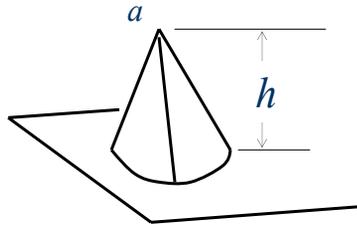
$$\delta = \int_0^L \frac{P_x}{EA_x} dx \quad (5)$$



Deformations of Members under Axial Loading

■ Example 6

- Determine the deflection of point a of a homogeneous circular cone of height h , density ρ , and modulus of elasticity E due to its own weight.



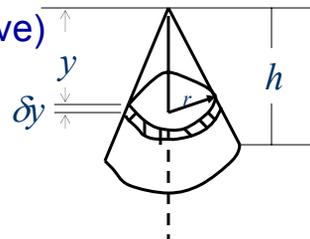
Deformations of Members under Axial Loading

■ Example 6 (cont'd)

- Consider a slice of thickness dy
- P = weight of above slice
- $= \rho g$ (volume above)

$$P = \rho g \left(\frac{1}{3} \pi r^2 y \right)$$

$$d\delta = \frac{P dy}{EA} = \frac{\rho g \left(\frac{1}{3} \pi r^2 y \right)}{E(\pi r^2)} = \frac{\rho g}{3E} y dy$$





Deformations of Members under Axial Loading

■ Example 6 (cont'd)

$$d\delta = \frac{\rho g}{3E} y dy$$

$$\delta = \int_0^h \frac{\rho g}{3E} y dy = \frac{\rho g}{3E} \frac{y^2}{2} \Big|_0^h$$

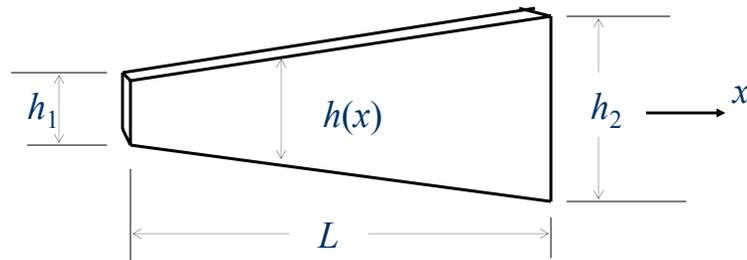
$$\delta = \frac{\rho g h^2}{6E} \downarrow$$



Deformations of Members under Axial Loading

■ Normal Stresses in Tapered Bar

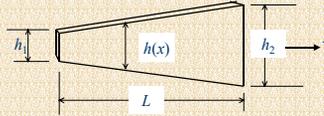
- Consider the following tapered bar with a thickness t that is constant along the entire length of the bar.





Deformations of Members under Axial Loading

■ Normal Stresses in Tapered Bar



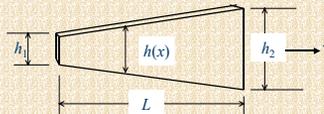
- The following relationship gives the height h of tapered bar as a function of the location x

$$h_x = h_1 + (h_2 - h_1) \frac{x}{L} \quad (6)$$



Deformations of Members under Axial Loading

■ Normal Stresses in Tapered Bar



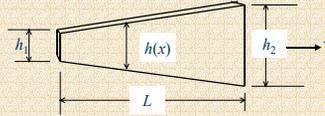
- The area A_x at any location x along the length of the bar is given by

$$A_x = th_x = t \left[h_1 + (h_2 - h_1) \frac{x}{L} \right] \quad (7)$$



Deformations of Members under Axial Loading

■ Normal Stresses in Tapered Bar



- The normal stress σ_x as a function of x is given

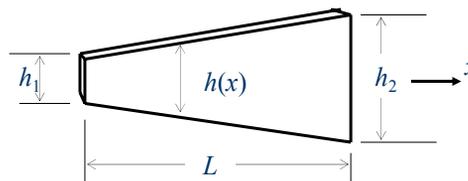
$$\sigma_x = \frac{P}{A_x} = \frac{P}{t \left[h_1 + (h_2 - h_1) \frac{x}{L} \right]} \quad (8)$$



Deformations of Members under Axial Loading

■ Example 7

- Determine the normal stress as a function of x along the length of the tapered bar shown if
- $h_1 = 2$ in
- $h_2 = 6$ in
- $t = 3$ in, and
- $L = 36$ in
- $P = 5,000$ lb





Deformations of Members under Axial Loading

■ Example 7 (cont'd)

- Applying Eq. 8, the normal stress as a function of x is given by

$$\sigma_x = \frac{P}{A_x} = \frac{P}{t \left[h_1 + (h_2 - h_1) \frac{x}{L} \right]}$$

$$\sigma_x = \frac{5000}{3 \left[2 + (6 - 2) \frac{x}{36} \right]} = \frac{5000}{6 + \frac{x}{3}}$$

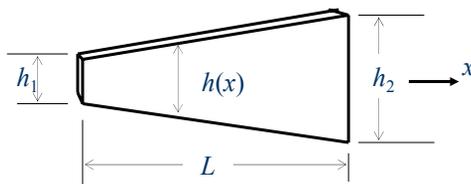
$$\sigma_x = \frac{15000}{18 + x}$$



Deformations of Members under Axial Loading

■ Example 7 (cont'd)

- Max $\sigma = 833.3$ psi
 - At $x = 0$
- Min $\sigma = 277.8$ psi
 - At $x = 36$ in

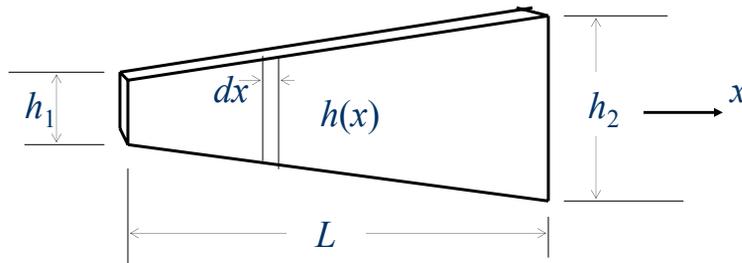


x (in)	σ (psi)
0	833.3
3	714.3
6	625.0
9	555.6
12	500.0
15	454.5
18	416.7
21	384.6
24	357.1
27	333.3
30	312.5
33	294.1
36	277.8



Deformations of Members under Axial Loading

- Deflection of Tapered Bar
 - Consider the following tapered bar with a thickness t that is constant along the entire length of the bar.



Deformations of Members under Axial Loading

- Deflection of Tapered Bar

- Recall Eq. 5

$$\delta = \int_0^L \frac{P_x}{EA_x} dx$$

- Substitute Eq. 7

$$P_x = P \left[\frac{h_2 - h_1}{L} x + h_1 \right]$$

- into Eq. 5, therefore

$$\delta = \frac{PL}{Et} \int_0^L \frac{1}{h_1 L + (h_2 - h_1)x} dx \quad (9)$$



Deformations of Members under Axial Loading

■ Deflection of Tapered Bar

Integrating Eq. 9, the deflection of a tapered bar is given by

$$\delta = \frac{PL}{Et} \left(\frac{1}{h_2 - h_1} \right) \ln[(h_2 - h_1)L] \quad (10)$$